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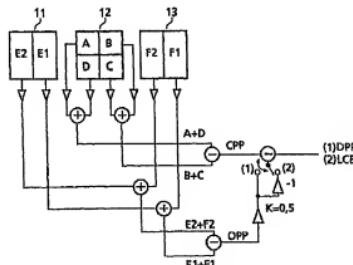
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(54) Title: METHOD FOR GENERATING A LENS POSITION SIGNAL AND CORRESPONDING APPARATUS FOR READING FROM AND/OR WRITING TO AN OPTICAL RECORDING MEDIUM



(57) Abstract: In order to generate a lens position signal (LCE), which describes the position of the optical axis of an objective lens (6) of an apparatus for reading from and/or writing to an optical recording medium (7) with regard to the optical axis of the remaining components (2, 3, 4, 5, 8, 9) contained in an optical scanner (21), the application of the DPP method is proposed in accordance with a first exemplary embodiment, wherein a primary-beam error signal (CPP) and a secondary-beam error signal (OPP) are obtained with the aid of the DPP method, wherein the desired lens position signal (LCE) is generated by addition of the primary-beam error signal (CPP) and the secondary-beam error signal (OPP). In accordance with a second exemplary embodiment, it is not necessary to generate a primary beam, rather it suffices to detect the secondary beams reflected from the optical recording medium (7) in order to obtain the lens position signal (LCE) by addition of the secondary-beam error signals (OPP1, OPP2) generated in a manner dependent thereon.

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METHOD FOR GENERATING A LENS POSITION SIGNAL AND
CORRESPONDING APPARATUS FOR READING FROM AND/OR WRITING
TO AN OPTICAL RECORDING MEDIUM

- 5 The present invention relates to a method for generating
a lens position signal, which describes the position of
the optical axis of an objective lens of an apparatus for
reading from and/or writing to an optical recording
medium with regard to the optical axis of an optical
10 scanner used in this apparatus, and also to a
correspondingly configured apparatus for reading from
and/or writing to an optical recording medium.

A track error signal is conventionally generated in
15 apparatuses for reading from and/or writing to optical
recording media, such as, for example, optical recording
media (e.g. DVD-RAM) in which information tracks are
contained both in depressions (G), designated as
"groove", and in elevations (L), designated as "land",
20 which track error signal can be used for tracking
regulation in the respective apparatus. One of the
widespread methods for forming the track error signal is
the so-called "differential push-pull" (DPP) method, as
is described for example in EP 0 745 982 A2. In this
25 case, the laser beam output by a laser diode is split
into three beams, namely a primary beam and two secondary
beams which scan mutually adjacent tracks of the optical
recording medium respectively used. The primary and
secondary beams reflected from the optical recording
30 medium are evaluated in order to obtain, in a manner
dependent thereon, primary-beam and secondary-beam track
error signals from which the desired track error signal
is generated by means of weighted combination.

- 35 A corresponding arrangement is illustrated by way of
example in Figure 8. The light emitted by a light source
or a laser 1 passes through a collimator lens 2 and is
then split into the primary beam (i.e. a 0th-order beam)

- and the two secondary beams (i.e. \pm 1st-order beams) by a diffraction grating 3. The primary beam, which reads the information to be scanned in a track of a corresponding recording medium 7, usually contains the majority 5 (approximately 80-90%) of the light information. The two secondary beams each contain the remaining 5-10% of the total light intensity, it being assumed for the sake of simplicity that the light energy of the higher orders of diffraction of the diffraction grating 3 is zero. These 10 three beams are focused onto the optical recording medium 7 via a polarizing beam splitter 4 and a quarter-wave plate 5 and also an objective lens 6, in order to read from and/or write to the said optical recording medium. The three beams reflected from the optical recording 15 medium 7 are fed via the beam splitter 4 and a cylindrical lens 8 to a photodetector unit 9, which detects the three beams reflected from the optical recording medium 7. The three beams are indicated symbolically in the figure between cylindrical lens 8 and 20 photodetector unit 9. Connected to the photodetector unit 9 is an evaluation unit 10, which evaluates the detected signals of the reflected primary and secondary beams for the purpose of generating a track error signal.
- 25 The diffraction grating 3 is incorporated in such a way that the imaging of the two secondary beams scans precisely the centre of the secondary tracks or (in the case of media which can be written to only in "groove" tracks) the centre beside the track scanned by the 30 primary beam. Since the secondary beams and the primary beam are intended to be optically separable from one another, the positions of their imaging on the optical recording medium 7 and on the photodetector unit 9 are separate from one another. If the optical recording 35 medium 7 rotates, then one of the secondary beams is situated in front of, and the other secondary beam behind, the primary beam in the reading or writing direction. The evaluation unit 10 of the arrangement

shown in Figure 8 evaluates the light intensities reflected onto the photodetector 9 separately for each of the three beams.

- 5 In the evaluation unit 10, the detected signals both of the primary beam and of the secondary beams are used to generate, considered by themselves in each case, a push-pull signal which represents the track error of the respective beam with respect to the track. However, since
10 the two secondary beams scan the secondary tracks with respect to the read/write track, their push-pull track error is inverted with respect to that of the primary beam. Considered by themselves, the respective push-pull components thus contain the actual track error with
15 respect to the respectively scanned track. Since the track position of the three beams can only change together, the three push-pull signals change equally.

The objective lens 6 of an optical scanner 21 as sketched
20 in Figure 8 must be mounted in a movable manner in order, even in the case of an optical recording medium 7 which has vertical wobble and/or eccentricity, to make it possible to focus the scanning beam and keep it on a predetermined track. That part of the scanner 21 which
25 comprises the elements 2, 3, 4, 5, 8, 9 defines an optical axis 22. The objective lens 6 is arranged in its rest position ideally in such a way that its optical axis
23 corresponds to the optical axis 22 of the other optical components of the optical scanner 21.

30 The movement of the objective lens 6 is usually achieved by means of an electromagnetic drive. In this case, the objective lens is kept in a predetermined rest position by an arrangement of articulated joints or springs, from
35 which position it can be deflected from its rest position by application of a current to the electromagnetic drive. To that end, the output signals of the evaluation unit 10 provide track error and focus error signals which

encompass the position of the objective lens 6 and correct it with the aid of regulating circuits.

If the intention is to scan an optical recording medium 7 whose tracks are applied in spiral form, then the objective lens 6 is deflected to an increasing extent during a continuous scanning operation. Its optical axis 23 is therefore displaced increasingly far from the optical axis 22 of the other optical components. In order 10 to counteract this displacement of the optical axes with respect to one another, provision is usually made of a servo or linear motor which subsequently shifts the scanner 21 with the optical components 2, 3, 4, 5, 8, 9 incorporated therein in such a way that the optical axes 15 deviate from one another as little as possible. This motor is usually referred to as coarse track motor. According to the prior art, the driving voltage of the electromagnetic drive of the objective lens is used as a criterion for the deviations of the optical axes and the 20 coarse track motor is driven in such a way that the driving voltage tends to zero.

For this purpose, provision is made of a further regulating circuit, which ensures that the optical axes 22, 23 of scanner 21 and objective lens 6 correspond. According to the prior art, the driving voltage of the electromagnetic drive of the objective lens 6 is evaluated for this purpose. In this case, it is assumed that the optical axis 23 of the objective lens 6 does not 25 deviate from the axis of the other components 22 when the drive coils are de-energized. Since the objective lens is suspended in a resilient fashion, this assumption is not correct in all operating situations. By way of example, the objective lens changes its position even without 30 driving of the drive coils if external forces act on it, as may occur in the event of an impact against the player. Furthermore, ageing of the articulated joints or 35 springs may cause the rest position of the objective lens

to be changed such that the optical axes deviate from one another. These effects cannot be detected from the driving voltage of the drive coils.

- 5 If the objective lens 6 is then moved for example during a track jump, the imaging of the primary and secondary beams on the photodetector unit 9 also moves. This displacement of the imaging results in an offset voltage at the output of the evaluation unit 10, the direction of
10 this offset voltage being identical for all of the beams. The displacement of the objective lens 6 thus gives rise to an offset voltage which does not originate from an actual track error and is therefore an interference. The genuine track error component and the undesirable lens-
15 movement-dependent component are added in the push-pull signal which is detected by the respective detectors of the photodetector unit 9 and yielded by the evaluation unit 10.
- 20 If the push-pull signals of the secondary beams are then added and this sum is subtracted from the push-pull signal of the primary beam, this undesirable lens-movement-dependence component is cancelled out given appropriate weighting between the primary and secondary
25 beam components. By contrast, since the push-pull components of primary and secondary beams are inverted with respect to one another, they are added in the correct phase after application of the subtraction, with the result that, given correct setting of the weighting
30 factor, the actual track error is obtained. A method for determining a suitable weighting factor is described by way of example in EP 0 708 961 B1.

From the previously described properties of the conventional DPP method, it is apparent that, owing to the position of the secondary beams, the phase shift between the primary beam and the secondary beams is nominally 180 degrees. This is advantageous since, as a

result of the difference formation, the track error components of the primary beam and of the secondary beams are added with the largest possible amplitude. If the position of the beams on the tracks is considered, then
5 the angle of the diffraction grating 3 is set, for achieving the maximum amplitude of the track error signal, precisely in such a way that (for example in the case of a DVD-RAM) the secondary beams impinge on the track centres of the secondary tracks or (in the case of
10 media which can be written to only in "groove" tracks) precisely on the region between two tracks beside the track scanned by the primary beam.

The aim of the DPP method described previously is to form
15 a track error signal which has no offset dependence on the position of the objective lens 6 relative to the optical axis of the scanner respectively used. In the case of the previously described combination of the push-pull components of the primary beam and of the secondary
20 beams, although the actual track error can be obtained, owing to the cancellation of the lens-movement-dependence component it is nonetheless not possible to detect the position of the objective lens 6 with regard to the optical axis of the scanner.
25

During a track following operation, the objective lens 6 is displaced perpendicularly to the track direction of the optical recording medium 7, i.e. the optical axis of the objective lens 6 is moved away from the optical axis
30 of the scanner 21. This results in a corresponding displacement of the imaging of the reflected scanning beam on the detector elements of the photodetector unit 9. While the respectively scanned track is followed correctly, the evaluation unit 10 cannot recognize in
35 this case that the optical axes of objective lens 6 and scanner 21 do not correspond. For this reason, it is necessary, in principle, to provide a signal which

describes the position of the objective lens 6 with regard to the optical axis 22 of the scanner 21.

It is furthermore advantageous, during a positioning 5 operation, as is necessary for example for an access to another piece of music on a CD, to provide for the control unit of the apparatus auxiliary signals which enable a fast access to the piece of music desired by the user of the apparatus.

10

An object of the present invention is to propose a method for generating a lens position signal, which describes the position of the objective lens with regard to the optical axis of an optical scanner, and also a 15 corresponding apparatus for reading from and/or writing to an optical recording medium.

Furthermore, possibilities for generating auxiliary signals for an improved track jump are shown.

20

This object is achieved according to the invention by means of a method having the features of Claim 1 or 11 and an apparatus having the features of Claim 20 or 27. The subclaims each define preferred and advantageous 25 embodiments of the present invention.

A first exemplary embodiment of the present invention proposes that the lens position signal be generated by employing the DPP method described in the introduction. 30 In contrast to the prior art described in the introduction, however, the push-pull signal of the secondary beams is added to the push-pull signal of the primary beam in order to obtain the lens-movement-dependent component. In this case, in particular, a 35 weighted addition is carried out, in which case the weighting factor can be set to an ideal value in a manner dependent on the distance between the two secondary beams and the primary beam and on the track spacing. In a

variant of the first exemplary embodiment, a normalization of the signals derived from the beams used is provided in order to simplify the setting of the weighting factor.

5

In accordance with a second exemplary embodiment of the present invention, the lens position signal is derived directly from the push-pull signals of the secondary beams, i.e. the push-pull signal of the primary beam is 10 in this case not included in the generation of the lens position signal. In this case, it is particularly advantageous if the secondary beams are imaged on the optical recording medium in accordance with the following formula:

15

$$\Delta x = (2n - 1) * \frac{p}{2} \quad \text{where } n = 0, 1, 2, \dots \quad (1)$$

In this case, Δx designates the distance between the secondary beams and the (imaginary or existing) primary beam and p designates the track spacing. In the latter, 20 the track error components of the push-pull signals of the two secondary beams cancel one another out, so that the resultant summation signal only comprises the lens-movement-dependent contribution and, consequently, corresponds to the desired lens position signal, which 25 can be used for example in the event of a track jump for stabilization of the actuator.

In the case of the previously described orientation of the secondary beams, it is additionally possible to 30 generate a direction signal from the phase between the difference signal of the two push-pull signals of the secondary beams and the push-pull signal of the primary beam. Equally, it is possible to generate a track error signal.

35

The present invention is explained in more detail below using preferred exemplary embodiments with reference to the accompanying drawings.

- Figure 1 shows a first exemplary embodiment of the present invention for generating a lens position signal,
- 5 Figure 2 shows a variant of the first exemplary embodiment shown in Figure 1,
- 10 Figure 3 shows a further variant of the first exemplary embodiment shown in Figure 1,
- 15 Figure 4 shows a track image with the beam arrangement of the primary beam and secondary beams and the push-pull signals obtained with this beam arrangement in accordance with a second exemplary embodiment of the present invention,
- 20 Figure 5 shows the second exemplary embodiment of the present invention for generating a lens position signal,
- 25 Figure 6 shows a beam arrangement of a primary beam and four secondary beams and also the push-pull signals obtained with this beam arrangement with a variant of the second exemplary embodiment,
- 30 Figure 7 shows, by way of example, a photodetector unit for detecting the reflected primary and secondary beams shown in Figure 6,
- 35 Figure 8 shows a simplified construction of an optical scanner for carrying out the DPP method according to the prior art, and this construction can also be applied to the present invention, and

Figure 9 to

Figure 12 show further variants of the first exemplary embodiment shown in Figure 3, a normalization being provided.

5

As was described in the introduction, the track error signal generated in accordance with the DPP method is composed of the corresponding component of the primary beam and the added components of the secondary beams, in 10 accordance with the prior art the components of the secondary beams being added and the resultant sum being subtracted from the component of the primary beam with appropriate weighting.

15 For all of the following considerations, it is assumed in a simplification that the intensities of the three scanning beams considered are identical when impinging on the photodetector unit 9. In practice, however, the intensity of the secondary beams is dependent on their 20 track position, on the reflection of the scanned track and also on the properties of the diffraction grating 3 and is weaker than the intensity of the primary beam, so that the intensity of the secondary beams has to be scaled correspondingly with respect to the primary beam 25 intensity. This can ideally be done by means of a normalization.

Under the above-described assumption, the following relationships hold true; in this respect, also see, for 30 example, Figure 4 described in more detail further below:

$$DPP = CPP - K * OPP \quad (2)$$

$$CPP = a * \sin\left(2\pi * \frac{x}{2p}\right) + k\ell \quad (3)$$

$$\begin{aligned} OPP &= a * \left(\sin\left(2\pi * \frac{x + \Delta x}{2p}\right) + \sin\left(2\pi * \frac{x - \Delta x}{2p}\right) \right) + k(\ell + \ell) \\ &= a * \left(\sin\left(2\pi * \frac{x + \Delta x}{2p}\right) + \sin\left(2\pi * \frac{x - \Delta x}{2p}\right) \right) + 2k\ell \end{aligned} \quad (4)$$

In this case, DPP designates the signal obtained in accordance with the DPP method, CPP designates the corresponding component of the primary beam, OPP 5 designates the component of the secondary beams, K designates a weighting factor, x designates the scanning position of a beam relative to the track centre, Δx designates the distance between the two secondary beams and the primary beam and p designates the track spacing, 10 which in this case, corresponding to the definition in accordance with the DVD-RAM standard, is measured between the centres of two adjacent tracks. ℓ designates the movement of the objective lens 6 from the rest position. The amplitudes a and k are factors which depend on the 15 geometry of the scanned tracks, the sensitivity of the photodetector unit 9, etc. Since the three beams are mechanically coupled to one another, the variables x and ℓ in the formulae for the CPP signal and the OPP signal are identical in each case.

20 In order to achieve compensation of the lens-movement-dependent component ℓ , the following equation must be satisfied:

$$25 \quad DPP_\ell = CPP_\ell - K * OPP_\ell = 0 \quad (5)$$

In this case, the index " ℓ " respectively designates the lens-movement-dependent component of the corresponding signal. Taking account of formulae (3) and (4) above, it 30 follows for the weighting factor for compensation of the lens-movement-dependent component that:

$$K = 0.5 \quad (6)$$

This weighting factor K is independent of the orientation 35 of the secondary beams with regard to the primary beam.

It is usually attempted to make the track error amplitude a maximum by setting the distance Δx accordingly. This is achieved, in the case of evaluation of formulae (2) to (4) above with $K = 0.5$, when the following relationship 5 holds true:

$$\cos\left(\pi * \frac{\Delta x}{p}\right) = -1 \quad (7)$$

Since the cosine function is periodic, this holds true for:

10

$$\Delta x = (2n + 1) * p \quad \text{where } n = 0, 1, 2, \dots \quad (8)$$

It follows from formulae (2) to (4) that when a new weighting factor G with a negative sign is used, i.e. 15 when the subtraction of the OPP signal from the CPP signal is replaced by an addition of these two signals, only the lens-movement-dependent component is retained, while the individual track error components cancel one another out. In particular, the following relationship 20 must hold true for compensation of the track error components:

$$DPP_x = CPP_x - G * OPP_x = 0 \quad (9)$$

25 In this case, the index "x" designates the track-error-dependent component of the respective signal. The relationship of (9) is satisfied taking account of relationships (3) and (4) above if the following holds true:

30

$$DPP_x = a * \sin\left(\pi * \frac{x}{p}\right) * \left(1 - 2G \cos\left(\pi * \frac{\Delta x}{p}\right)\right) = 0 \quad (10)$$

The track-error-dependent component of the DPP signal can thus be eliminated in a manner dependent on Δx and p if the following holds true:

$$1 - 2G \cos\left(\pi * \frac{\Delta x}{p}\right) = 0 \quad (11)$$

Given an assumed distance between the secondary beams and the primary beam of $\Delta x = p$, the following results in this respect:

5

$$G = -0.5 \quad (12)$$

From the negative sign of the weighting factor G in accordance with formula (12), it emerges that the subtraction must be replaced by an addition. If the secondary beams are arranged at $\Delta x = p$, the application of the addition of the CPP and OPP signals thus suffices to make the track error components tend to zero and to obtain the lens-movement-dependent component. With $G = -0.5$, by inserting $\Delta x = p$ into formulae (2) to (4), the lens-movement-dependence component is obtained as follows:

20

$$DPP_t = 2kl \quad (13)$$

The signal thus obtained contains only the lens-movement-dependent component; it is designated by LCE (Lens Centre Error).

25

Figure 1 illustrates a corresponding exemplary embodiment for generating the lens-movement-dependent component for the corresponding lens position signal LCE by employing the DPP method. In this case, it is assumed that the photodetector unit 9 for detecting the reflected primary beam has a photodetector unit 12 having four photosensitive areas A - D, while respective photodetector elements 11, 13 having only two photosensitive areas E1, E2 and F1, F2, respectively, are provided for detecting the reflected secondary beams. As can be seen from Figure 1, provision is made of an amplifier having a gain factor -1 and, in order to change over from track regulation operation to lens position

.

control, a switch, the signals CPP and 0.5 · OPP being either subtracted or added depending on the switch position.

- 5 In order to be able to measure the lens position during the playback operation of the optical recording medium 7, it is necessary simultaneously to form the track error signal DPP from the difference and also the lens position signal LCE from the sum of the partial signals CPP and
10 OPP. Figure 2 shows a corresponding variant of the exemplary embodiment shown in Figure 1. Since both signals are available simultaneously in this case, the track regulating circuit can be closed and, at the same time, the information about the lens position can be used
15 for readjusting the coarse track motor of the optical scanner 21.

If the distance Δx between the secondary beams and the primary beam is not $\Delta x = p$ but rather $\Delta x = 3/4p$, for
20 example, the following results for the weighting factor G, which leads to the compensation of the track error component, in accordance with formula (11):

$$G = -\frac{1}{\sqrt{2}} \quad (14)$$

- 25 In this case, the optimum weighting factor K for generating the track error signal differs from the weighting factor G required for generating the lens position signal not only in terms of sign but also in terms of magnitude. The weighting factor K for
30 suppressing the lens-movement-dependent component is ideally always 0.5, while the weighting factor for compensation of the track error component is always negative, but is to be adapted to the position of the secondary beams. Accordingly, the arrangement shown in
35 Figure 2 can be modified as shown in Figure 3, in which case the weighting factor used for generating the lens position signal LCE can be set in a variable manner.

If a variably adjustable weighting factor is provided, secondary track distances Δx different from those mentioned above can also be used in conjunction with the DPP track error method. Track distances in the range of 5 $p/2 < \Delta x < 3p/2$ can theoretically be utilized. The limits $p/2$ and $(3/2)*p$ cannot be utilized in practice since the track error contribution in the signal component OPP becomes zero here and, even given an infinitely large factor G set, compensation of the track error 10 contribution of the CPP signal could not be achieved. Instead, it is possible here to use the sum of the signals OPP1 and OPP2 alone in order to obtain a lens position signal. This is illustrated in the following section and also in Figures 4 and 5. If the formation of 15 a track error signal according to the DPP method is disposed with, then the lens position signal can also be formed with arbitrary secondary track distances Δx . Limiting cases emerge here as $\Delta x = 0$ or $\Delta x = 2 \cdot n \cdot p$, since the track-error-dependent components of the partial 20 signals CPP, OPP1 and OPP2 are in phase here and compensation of these components cannot be achieved. Furthermore, it should be noted that the sign of the weighting factor G is reversed for $0 < \Delta x < p/2$ and also for $3p/2 < \Delta x < 2p$.

25 The previously described method for generating the lens position signal LCE using the DPP method is suitable, in particular, for all optical recording media which, on account of their physical construction, are suitable for 30 application of the DPP method if, at the same time, a track error signal is intended to be generated. However, the position of the optical axis of an objective lens with regard to the optical axis of an optical scanner can also be ascertained if the optical recording medium 7 is 35 not suitable for application of the DPP method. Corresponding examples of this will be explained below.

The lens position signal LCE can be formed, for example, in accordance with a further exemplary embodiment, if the secondary beams are imaged with the following distance Δx :

5

$$\Delta x = (2n - 1) * \frac{p}{2} \text{ where } n = 0, 1, 2, \dots \quad (15)$$

The consequence of this is that the track error components of the two secondary beams $OPP1 = (E2 - E1)$ 10 and $OPP2 = (F2 - F1)$ cancel one another out and their magnitude with respect to the track error signal becomes zero. This means that the summation signal OPP yields only the contribution dependent on the lens movement ℓ and, consequently, corresponds directly to the lens 15 position signal LCE.

As is shown in Figure 4, a scanner which uses a three-beam track error signal for track regulation typically has two secondary beams 15, 16, which are imaged on the 20 optical recording medium with $\Delta x = p/2$ beside the primary beam 14. In this case, Δx is measured in the direction of the imaginary x-axis depicted, whose origin lies in the centre of the scanning spot of the primary beam 14, in this case in the centre of a track. As is also shown in 25 Figures 1 to 3, the photodetectors used for detecting the reflected secondary beams 15, 16 are in each case divided into two parts in order simultaneously to obtain a track error signal and a lens position signal. The separation of the photodetector areas is such that the beams 30 reflected from the optical recording medium impinge symmetrically with respect to the separating line.

Figure 4 illustrates a track image for such a beam arrangement of the secondary beams with $\Delta x = p/2$ and also 35 the resultant track error signals. A corresponding arrangement for obtaining the signals illustrated in Figure 4 is shown in Figure 5.

- As can be seen from Figure 4, the track error components of the two secondary beam signals OPP1 and OPP2 cancel one another out, so that the summation signal OPP = OPP1 + OPP2 yields only the contribution dependent on the lens movement ℓ and, consequently, corresponds to the desired lens position signal LCE. With this orientation of the secondary beams, it is additionally possible to generate a direction signal DIR from the phase between the difference signal
- 10 OPP1 - OPP2 and the CPP signal with the aid of a phase comparator shown in Figure 5, since the phase of these two signals with respect to one another is $+90^\circ$ or -90° depending on the direction of movement. A track error signal TE is likewise available which, however, has only
- 15 half the amplitude of the ideal DPP signal. Moreover, as is shown in Figure 5, it is possible to obtain a so-called "Track Zero Cross" signal TZC and also the information of what type of track (groove or land) the scanning beam is presently scanning.
- 20 The track zero cross signal TZC is obtained from the signal CPP by means of a comparator in Figure 5. Instead of this, as an alternative it may also be obtained from the corrected signal DPP. Another alternative, not
- 25 illustrated here, provides for only one of the signals OPP1 or OPP2 to be used, instead of the difference OPP1 - OPP2. This obviates the difference formation; the signal fed to the comparator then has only half the amplitude, as can be seen from Figure 4.
- 30 By means of a corresponding configuration of the diffraction grating 3 shown in Figure 8, it is also possible to direct onto the optical recording medium 7 only two or, alternatively, more than three beams in such
- 35 a way that at least one of the beams impinges on a "groove" track and generates a corresponding track error signal, while another beam impinges on a "land" track and likewise generates a corresponding track error signal

which is phase-shifted through 180° with respect to the track error signal of the first-mentioned beam. If these two signals are added to one another, then the track error component contained therein is likewise cancelled 5 out, and all that remains is the component dependent on the lens movement ℓ of the objective lens 6.

Furthermore, the present invention can also be applied to scanners with holographic optical components, provided 10 that two (secondary) beams are generated which impinge on the optical recording medium 7 at a distance of $\Delta x = (2n-1) \cdot p/2$ from an (imaginary or existing) primary beam and whose imaging on a correspondingly configured photodetector unit 9 or an evaluation unit 10 generates 15 two push-pull signals which have a phase shift of 180° with regard to their track error component, provided that the components proportional to the lens movement are added in the correct phase.

20 This is realized for example in a five-beam scanner, the ± 1 st-order secondary beams in each case impinging on the edges between a "groove" and a "land" track, while the ± 2 nd-order secondary beams impinge on the track centres of the adjacent tracks of the primary beam. A 25 corresponding track image is illustrated in Figure 6, the primary beam again being provided with the reference symbol 14, the 1st-order secondary beams being provided with the reference symbols 15, 16 and the 2nd-order secondary beams being provided with the reference symbols 17, 18. The distance between the 1st-order secondary beams 15, 16 and the primary beam 14 is thus $\Delta x_1 = p/2$, while the distance between the 2nd-order secondary beams 30 17, 18 and the primary beam 14 is $\Delta x_2 = p$.

35 Figure 7 illustrates an exemplary embodiment of the individual photodetectors 11-13 and 19, 20 of the photodetector unit, which each serve for detecting a beam 14-18 reflected from the corresponding optical recording

medium. In this case, the primary beam 14 is detected by a photodetector element 12 having four light-sensitive areas A-D, while the secondary beams are in each case detected by photodetector elements 11, 13, 19 and 20, respectively, having two light-sensitive areas E1, E2, F1, F2, G1, G2 and H1, H2, respectively. From the output signals of the light-sensitive areas of the individual photodetector elements, the following push-pull signals are again determined by an evaluation unit, which signals are illustrated by way of example in the lower part of Figure 6:

$$CPP = (A + D) - (B + C) \quad (16)$$

$$15 \quad OPP1 = E2 - E1 \quad (17)$$

$$OPP2 = F2 - F1 \quad (18)$$

$$OPP3 = G2 - G1 \quad (19)$$

$$20 \quad OPP4 = H2 - H1 \quad (20)$$

A DPP signal is formed for example from the difference between the signal of the primary beam, i.e. the CPP signal, and the summation signal of the 2nd-order secondary beams, as follows:

$$DPP = CPP - K * (OPP3 + OPP4) \quad (21)$$

30 The sum of the push-pull signals of the two first-order secondary beams again yields a voltage which is proportional to the lens movement ℓ of the objective lens, without a track error contribution, since the track error components, as described above, cancel one another 35 out, so that the desired lens position signal can be derived directly from this summation signal:

$$LCE = OPP1 + OPP2 \quad (22)$$

In addition, a direction signal indicating the direction with which the scanning beam crosses the tracks with the track regulating circuit open can be derived from the phase relationship of the push-pull signal of one of the 5 secondary beams 15-18 with respect to the push-pull signal of the primary beam 14.

As has already been mentioned in the introduction, for all the above considerations, it was assumed in a 10 simplification that the intensities of the three scanning beams considered are identical when impinging on the photodetector unit 9. The compensation factors G and K respectively specified therefore apply only if this simplification is employed.

15

In practice, however, the intensity of the secondary beams is dependent on their track position, on the reflection of the scanned track and also on the properties of the optical diffraction grating 3 and is 20 weaker than the intensity of the primary beam, so that the intensity of the secondary beams has to be scaled correspondingly with respect to the primary beam intensity. Ideally, this is done by means of a normalization. To that end, the signals derived from the 25 reflected beams are normalized. The signals CPP and OPP or, as an alternative, the individual signals OPP1 and OPP2 are normalized by dividing these signals by the summation signals which are proportional to the quantity of light respectively taken up by the detector areas. 30 Such a normalization is realized for example in the evaluation unit 10.

Proceeding from the exemplary embodiment shown in Figure 3, Figures 9 and 10 show two variants of a normalization. 35 Figure 9 shows an exemplary embodiment of a normalization in each case for the primary beam (CPP) and jointly for the secondary beams (OPP). In this case, the normalized signals are designated as CPPN, OPPN, LCEN and DPPN using

an appended "N". Figure 10 shows an exemplary embodiment in which the push-pull components of the three beams are normalized separately before the signals LCE and DPP are formed therefrom by weighted addition and subtraction, 5 respectively.

As described above, it is necessary to adapt the weighting factor G to the secondary track spacings. By way of example, if the variant shown in Figure 9 is taken 10 as a basis, then the signal amplitude of the signal LCE is dependent on the setting of the compensation factor G. This is avoided by a further variant of the variants shown in Figures 9 and 10, which is described below.

15 The variant shown in Figures 11 and 12, respectively, relates to the weighting between primary beam and secondary beams. It is advantageous, for example, to replace the weighting factor G for the secondary beam signal by two weighting factors G' and 1-G', which act on 20 the primary and secondary beam signals, where G' can be calculated from G according to the following relationships:

$$G' = \frac{G}{(1+G)} \quad (23)$$

25 What is achieved by splitting the weighting factor G into two weighting factors dependent on G' is that the amplitude of the lens-movement-dependent signal LCE is independent of the respective weighting factor to be set. In an analogous manner, formula (23) can also be applied 30 to the weighting factor K for forming the DPP signal. The factors G and K are chosen for example analogously to Figure 9 and Figure 10, respectively. The signals weighted in this way are designated by LCEN' and DPPN'.

PATENT CLAIMS

- 1) Method for generating a lens position signal,
 - 5 - wherein the lens position signal (LCE) describes the position of the optical axis (23) of an objective lens (6) of an apparatus for reading from and/or writing to an optical recording medium (7) with regard to the optical axis (22) of an optical scanner (21) assigned to the objective lens (6),
 - 10
 - 15 - wherein primary and secondary scanning beams (14-18) incident on adjacent tracks of the recording medium (7) are generated and the primary and secondary scanning beams reflected from the recording medium (7) are detected, and
 - 20
 - 25 - wherein a primary-beam error signal (CPP) and a secondary-beam error signal (OPP) are derived from the detected reflected primary and secondary scanning beams, characterized in that the lens position signal (LCE) is obtained by combination, in particular addition, of the primary-beam error signal (CPP) and the secondary-beam error signal (OPP).
- 2) Method according to Claim 1, characterized in that the lens position signal (LCE) is obtained by weighted combination of the primary-beam error signal (CPP) and secondary-beam error signal (OPP).
 - 30
 - 35
- 3) Method according to Claim 2, characterized in that the lens position signal (LCE) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with the following relationship:

$$LCE = CPP - G * OPP,$$

- wherein the weighting factor (G) is chosen in such a way that the following holds true:

$$1 - 2G \cos\left(\pi * \frac{\Delta x}{p}\right) = 0$$

5

- wherein Δx designates the distance between the secondary beams and the primary beam and p designates the track spacing of the optical recording medium (7).

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4) Method according to Claim 3, characterized in that the weighting factor (G) is set variably in a manner dependent on the distance between the secondary beams and the primary beam and the track spacing of the optical recording medium (7).

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5) Method according to one of Claims 1-4, characterized in that, in order to form the lens position signal (LCE), a normalization is applied to the primary-beam error signal (CPP) and the secondary-beam error signal (OPP).

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6) Method according to one of the preceding claims, characterized in that the lens position signal (LCE) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with the following relationship:

$$LCE = (1 - G') * CPP - G' * OPP \quad \text{mit} \quad G' = \frac{G}{(1 + G)},$$

30

wherein G describes a weighting factor.

7) Method according to one of the preceding claims, characterized in that a track error signal (DPP) is additionally obtained by subtraction of the

secondary-beam error signal (OPP) from the primary-beam error signal (CPP).

- 8) Method according to Claim 7, characterized in that
5 the track error signal (DPP) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP), in which the lens-movement-dependent component tends to zero by setting a suitable compensation factor (K), formed according
10 to the following relationship:

$$DPP = CPP - K * OPP.$$

- 9) Method according to Claim 7 or 8, characterized in that, in order to form the track error signal (DPP),
15 a normalization is applied to the primary-beam error signal (CPP) and the secondary-beam error signal (OPP), and in that this normalization is simultaneously used to form the lens position signal
20 (LCE).

- 10) Method according to one of Claims 7-9, characterized in that the track error signal (DPP) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with
25 the following relationship:

$$DPP = (1 - K') * CPP - K' * OPP \quad \text{mit} \quad K' = \frac{K}{(1 + K)},$$

wherein K describes a compensation factor.

- 30 11) Method for generating a lens position signal,

- 35 - wherein the lens position signal (LCE) describes the position of the optical axis (23) of an objective lens (6) of an apparatus for reading from and/or writing to an optical recording medium (7) with regard to the optical axis (22) of an

- optical scanner (21) assigned to the objective lens (6),
- 5 - wherein beams (15-18) incident on different tracks of the recording medium (7) are generated and the beams reflected from the recording medium (7) are detected, and
- 10 - wherein a respective error signal (OPP1, OPP2) is derived from the detected reflected beams, characterized in that the lens position signal (LCE) is obtained by addition of the error signals (OPP1, OPP2).
- 15 12) Method according to Claim 11, characterized in that a first beam reflected from the optical recording medium (7) is detected by a first photodetector (11) having two detector areas and a second beam reflected from the optical recording medium (7) is detected by a second photodetector (13) having two detector areas,
- 20 - in that a first error signal $OPP1 = E2 - E1$ and a second error signal $OPP2 = F2 - F1$ are obtained from the output signals $E1, E2$ of the first photodetector (11) and the output signals $F1, F2$ of the second photodetector (13), respectively, and
- 25 30 - in that the lens position signal (LCE) is obtained by addition of the two error signals (OPP1, OPP2).
- 35 13) Method according to Claim 11 or 12, characterized in that at least two secondary beams are imaged onto the optical recording medium (7) with a distance of $\Delta x = (2n - 1) \cdot p/2$ where $n = 0, 1, 2 \dots$ to form an additionally generated or imaginary primary beam, wherein p describes the track spacing on the optical

recording medium (7), and in that the lens position signal (LCE) is obtained by addition of the error signals (OPP1, OPP2) generated from the two secondary beams.

5

- 14) Method according to Claim 13, characterized in that a primary beam is additionally generated on the recording medium (7) and the primary beam reflected from the optical recording medium (7) is detected in order to derive a corresponding error signal (CPP) from the detected reflected primary beam, and in that a direction signal (DIR) describing the direction of movement of the objective lens (6) is derived from the phase between one of the error signals (OPP1, OPP2) derived for the two secondary beams and the error signal (CPP) derived for the primary beam.
- 15) Method according to Claim 13 or 14, characterized in that a primary beam is additionally generated on the recording medium (7) and the primary beam reflected from the optical recording medium (7) is detected, and in that a signal stating what type of track the primary beam is presently scanning is derived from one of the error signals (OPP1, OPP2) derived from the two secondary beams.
- 16) Method according to one of Claims 11-15, characterized in that, in order to form the lens position signal (LCE), a normalization is applied to the respective error signals (OPP1, OPP2).
- 17) Method according to one of Claims 11-16, characterized in that two secondary scanning beam pairs and a primary beam are generated, the secondary scanning beams and the primary beam being incident on adjacent tracks of the optical recording medium (7),

- in that the secondary scanning beams reflected from the optical recording medium (7) and the reflected primary scanning beam are detected and reflected secondary-beam error signals (OPP1-OPP4) and a primary-beam error signal (CPP) are derived therefrom, and
 - in that the lens position signal (LCE) is derived by addition of the secondary-beam error signals (OPP1, OPP2) of one secondary beam pair, while a track error signal (DPP) is derived from the secondary-beam error signals (OPP3, OPP4) of the other secondary beam pair and the primary-beam error signal (CPP) by addition of the corresponding secondary-beam error signals (OPP3, OPP4) and then weighted subtraction from the primary-beam error signal (CPP).
- 20 18) Method according to Claim 17, characterized in that a directional signal (DIR) describing the direction of movement of the objective lens (6) is derived from the phase between one of the secondary-beam error signals (OPP1-OPP4) and the primary-beam error signal (CPP).
- 25 19) Method according to Claim 17 or 18, characterized in that a signal yielding a statement about what type of track the primary beam is presently scanning is derived from one of the secondary-beam error signals (OPP1-OPP4), derived from the secondary beams.
- 30 20) Apparatus for reading from and/or writing to an optical recording medium,
- 35 - having a beam generating unit (1-3) for generating primary and secondary scanning beams incident on

adjacent tracks on the optical recording medium (7),

- having a photodetector unit (9) for detecting the primary and secondary scanning beams reflected from the optical recording medium (7), and
- having an evaluation unit (10) for forming a primary-beam error signal (CPP) and a secondary-beam error signal (OPP) from the detected primary and secondary scanning beams, characterized in that the evaluation unit (10) is configured in such a way that it generates a lens position signal (LCE), which describes the position of the optical axis of an objective lens (6) of the apparatus with regard to the optical axis of an optical scanner (21) - assigned to the objective lens (6) - of the apparatus, by combination, in particular addition, of the primary-beam error signal (CPP) and secondary-beam error signal (OPP).

- 21) Apparatus according to Claim 20, characterized in that the evaluation unit (10) is configured in such a way that it generates the lens position signal (LCE) in a manner dependent on the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with the following relationship:

30

$$LCE = CPP - G * OPP,$$

- wherein G describes a weighting factor which is chosen in such a way that the following holds true:

$$1 - 2G \cos\left(\pi * \frac{\Delta x}{p}\right) = 0,$$

- wherein Δx describes the distance between the secondary beams and the primary beam and p describes the track spacing on the optical recording medium (7).

5

- 22) Apparatus according to Claim 20 or 21, characterized in that the evaluation unit (10) is configured in such a way that, in order to form the lens position signal (LCE), it applies a normalization to the primary-beam error signal (CPP) and the secondary-beam error signal (OPP).
- 10 23) Apparatus according to one of Claims 20-22, characterized in that the lens position signal (LCE) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with the following relationship:
- 15

$$LCE = (1 - G') * CPP - G' * OPP \quad \text{where} \quad G' = \frac{G}{(1 + G)},$$

20 wherein G describes a weighting factor.

- 24) Apparatus according to one of Claims 20-23, characterized in that the evaluation unit (10) is configured in such a way that it additionally obtains a track error signal (DPP) by subtraction of the secondary-beam error signal (OPP) from the primary-beam error signal (CPP), in which track error signal the lens-movement-dependent component tends to zero by setting a suitable compensation factor K , formed according to the following relationship:
- 25

$$DPP = CPP - K * OPP.$$

- 30 35 25) Apparatus according to Claim 24, characterized in that the evaluation unit (10) is configured in such a way that, in order to form the track error signal

(DPP), it applies a normalization to the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) and simultaneously uses this normalization to form the lens position signal (LCE).

- 5 26) Apparatus according to Claim 24 or 25, characterized in that the track error signal (DPP) is obtained from the primary-beam error signal (CPP) and the secondary-beam error signal (OPP) in accordance with the following relationship:

$$\text{DPP} = (1 - K') * \text{CPP} - K' * \text{OPP} \quad \text{where } K' = \frac{K}{(1+K)}$$

- 10 15 27) Apparatus for reading from and/or writing to an optical recording medium,

- 20 - having a beam generating unit (1-3) for generating beams incident on different tracks on the optical recording medium (7),
- 25 - having a photodetector unit (9) for detecting the beams reflected from the optical recording medium (7), and
- 30 - having an evaluation unit (10) for generating error signals (OPP1, OPP2) corresponding to the reflected beams, characterized in that the evaluation unit (10) is configured in such a way that it generates a lens position signal (LCE), which describes the position of the optical axis of an objective lens (6) of the apparatus with regard to the optical axis of an optical scanner (21) assigned to the objective lens (6), by addition of the error signals (OPP1, OPP2).

- 28) Apparatus according to Claim 27, characterized in that the beam generating unit (1-3) generates a first and a second beam,
- 5 - in that the photodetector unit (9), for detecting the first and second beams reflected from the optical recording medium (7) respectively has a photodetector (11, 13) having two detector areas, and
- 10 - in that the evaluation unit (10) is configured in such a way that it generates a first error signal $OPP1 = E2 - E1$ from the output signals $E1, E2$ of the first photodetector (11) and a second error signal $OPP2 = F2 - F1$ from the output signals of the second photodetector (13) and obtains the lens position signal (LCE) by addition of the two error signals $OPP1 + OPP2$.
- 15
- 20 29) Apparatus according to Claim 27 or 28, characterized in that the beam generating unit (1-3) generates a first secondary beam and a second secondary beam with a distance of $\Delta x = (2n - 1) \cdot p/2$, where $n = 0, 1, 2 \dots$, to an additionally generated or imaginary primary beam, p describing the track spacing on the optical recording medium (7), and in that the evaluation unit (10) is configured in such a way that it generates a first error signal (OPP1) and a second error signal (OPP2) from the first and second secondary beams reflected from the optical recording medium (7) and obtains the lens position signal (LCE) by addition of the first and second error signals (OPP1, OPP2).
- 25
- 30
- 35 30) Apparatus according to Claim 29, characterized in that the beam generating unit (1-3) generates a primary beam incident on the optical recording

medium (7), and in that the evaluation unit (10) is configured in such a way that it generates a primary-beam error signal (CPP) in a manner dependent on the primary beam reflected from the optical recording medium (7), and derives a direction signal (DIR) which describes the direction of movement of the objective lens (6), from the phase between the difference signal of the error signals (OPP1, OPP2) generated for the two secondary beams and the primary-beam error signal (CPP).
5
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- 31) Apparatus according to Claim 29 or 30, characterized in that the beam generating unit (1-3) generates a primary beam incident on the optical recording medium (7), and in that the evaluation unit (10) is configured in such a way that it derives, from one of the secondary-beam error signals (OPP1-OPP4) derived from the secondary beams, a signal containing a statement about what type of track the primary scanning beam is presently scanning.
15
20
- 32) Apparatus according to one of Claims 27-31, characterized in that the evaluation unit (10) is configured in such a way that, in order to form the lens position signal (LCE), it applies a normalization to the respective secondary-beam error signals (OPP1, OPP2).
25
- 33) Apparatus according to one of Claims 27-32, characterized in that the beam generating unit (1-3) generates two secondary scanning beam pairs and a primary beam, the primary beam and the secondary beams being incident on adjacent tracks of the optical recording medium (7), and in that the evaluation unit (10) is configured in such a way that it derives a primary-beam error signal (CPP) and corresponding secondary-beam error signals (OPP1-OPP4) from the primary and secondary scanning
30
35

beams reflected from the optical recording medium (7), the evaluation unit (10) generating the lens position signal (LCE) by addition of the secondary-beam error signals (OPP1, OPP2) of one secondary beam pair, and generating a track error signal (DPP) by weighted subtraction of the sum of the secondary-beam error signals (OPP3, OPP4) of the other secondary beam pair from the primary-beam error signal (CPP).

- 10 34) Apparatus according to Claim 33, characterized in that the evaluation unit (10) is configured in such a way that, in order to form the lens position signal (LCE), it applies a normalization to the primary-beam error signal (CPP) and the secondary-beam error signals (OPP1, OPP2) of one secondary beam pair and, in order to form the track error signal (DPP), it applies a normalization to the primary-beam error signal (CPP) and the secondary-beam error signals (OPP3, OPP4) of the other secondary beam pair.
- 15
- 20

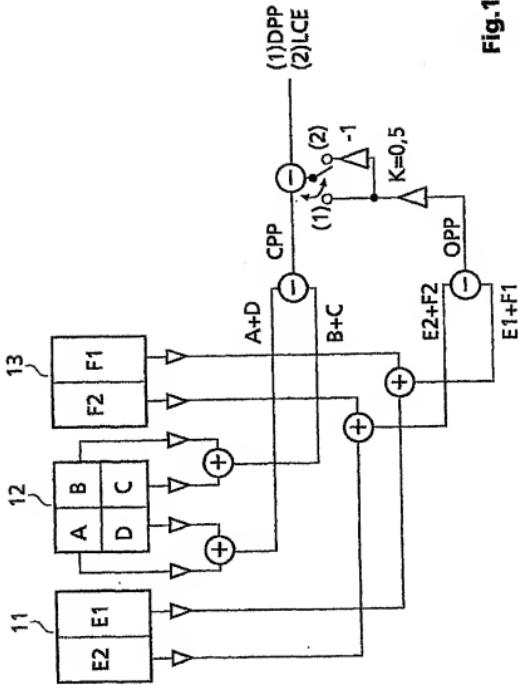
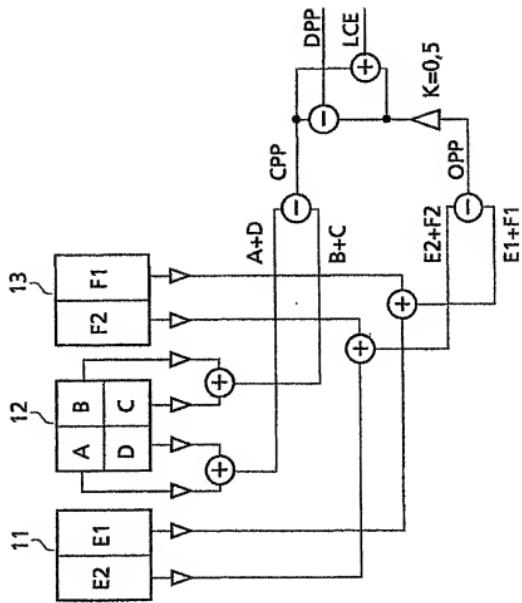
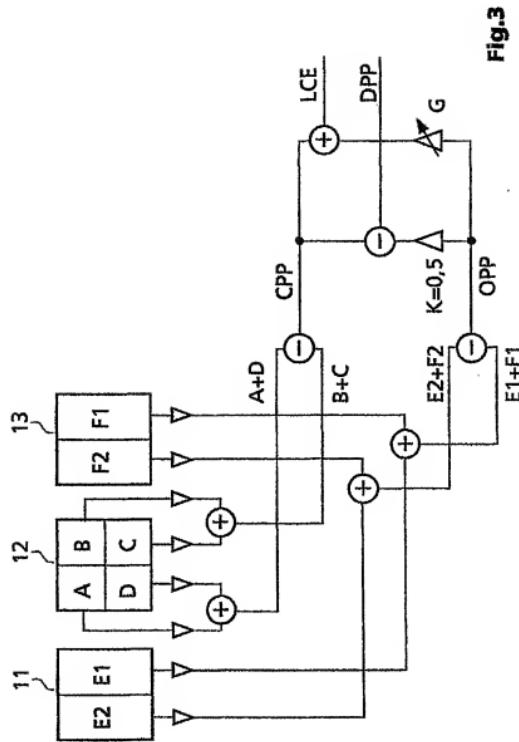


Fig.1

Fig.2





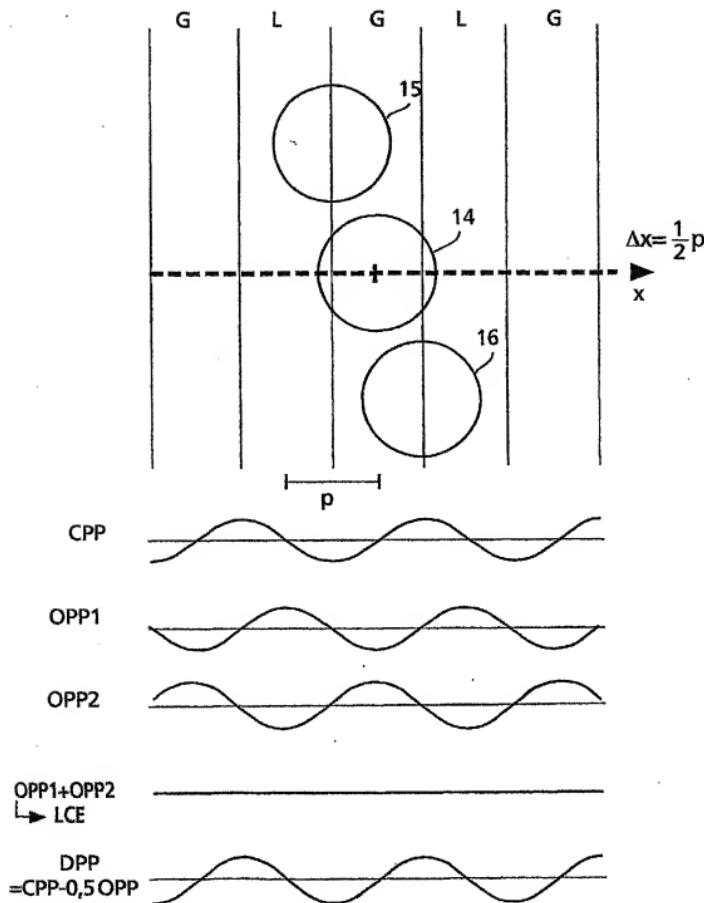


Fig.4

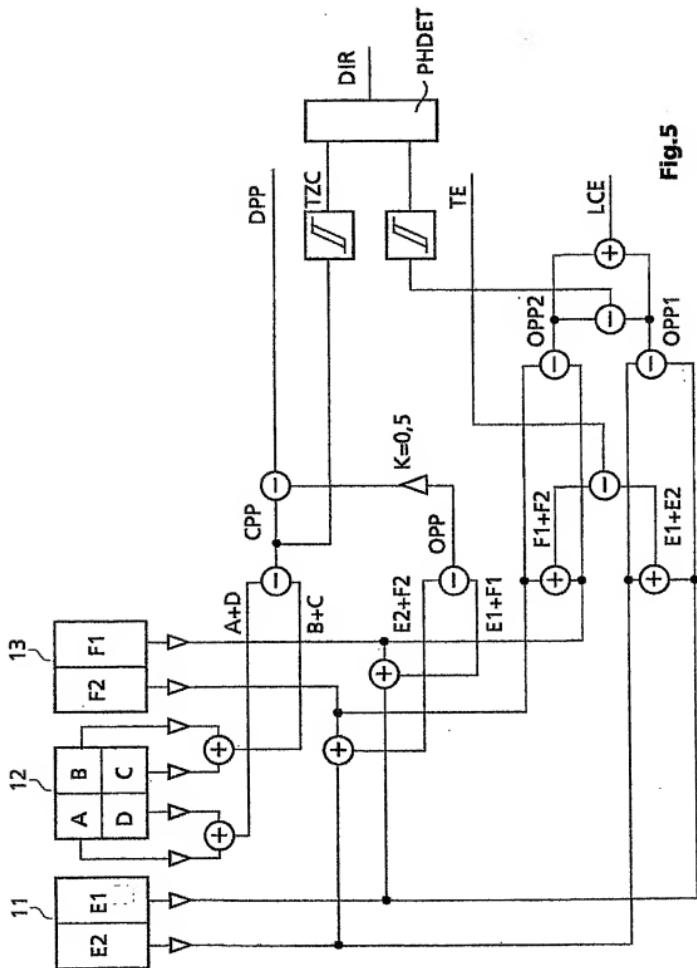


Fig.5

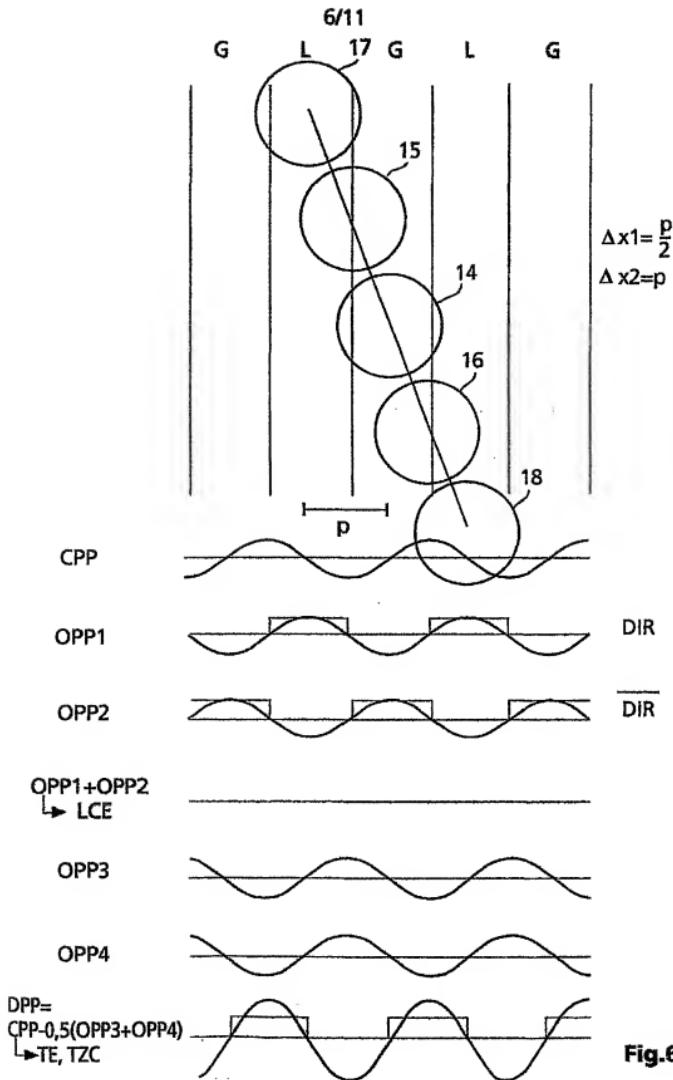


Fig.6

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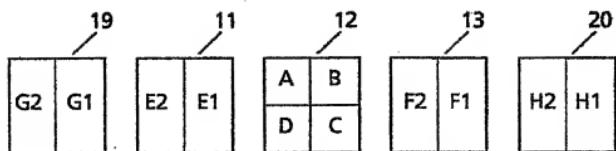


Fig.7

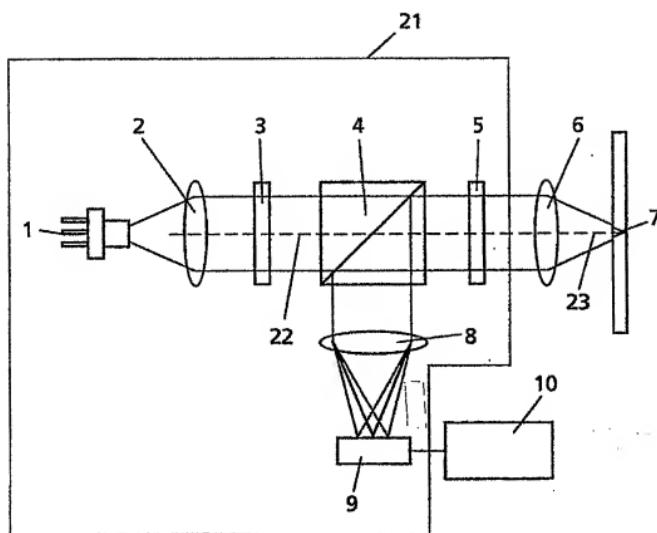
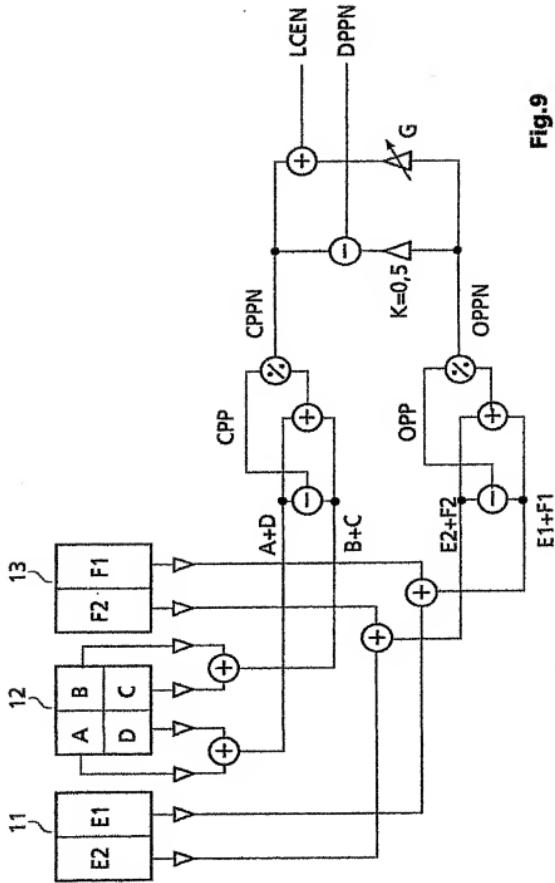


Fig.8

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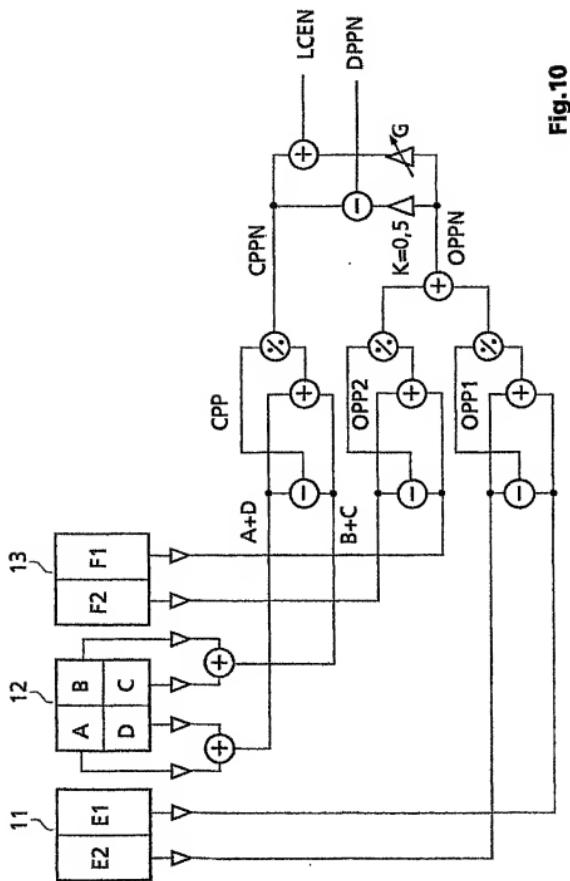


Fig. 10

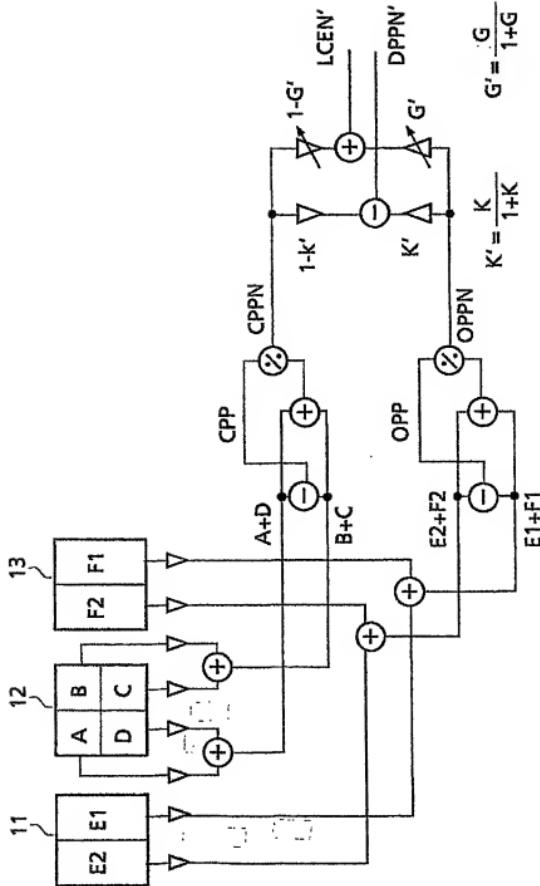


Fig.11

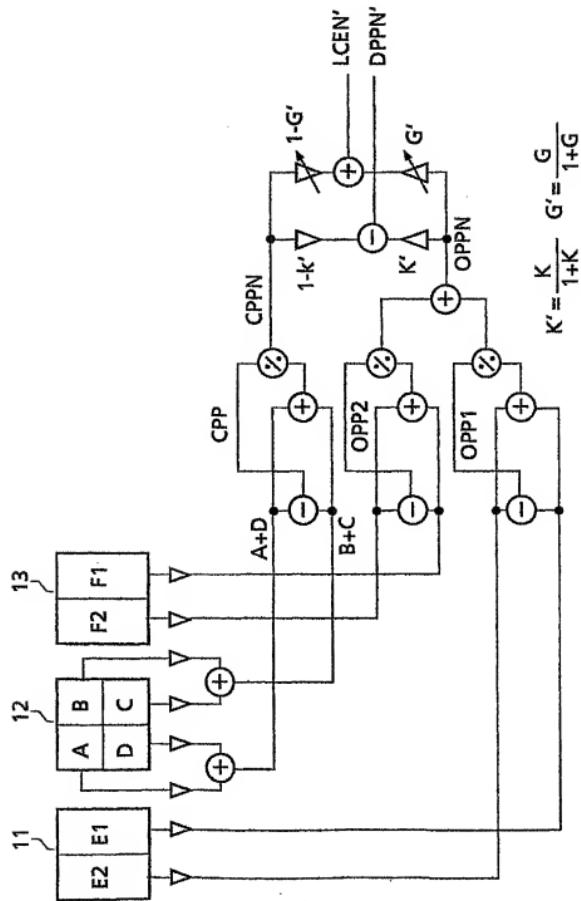


Fig.12